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RINA
GROUP

Industrial case study Nabucco pipeline Risk analysis

InnHF Zeroing course
Torino 22-25/January/2013

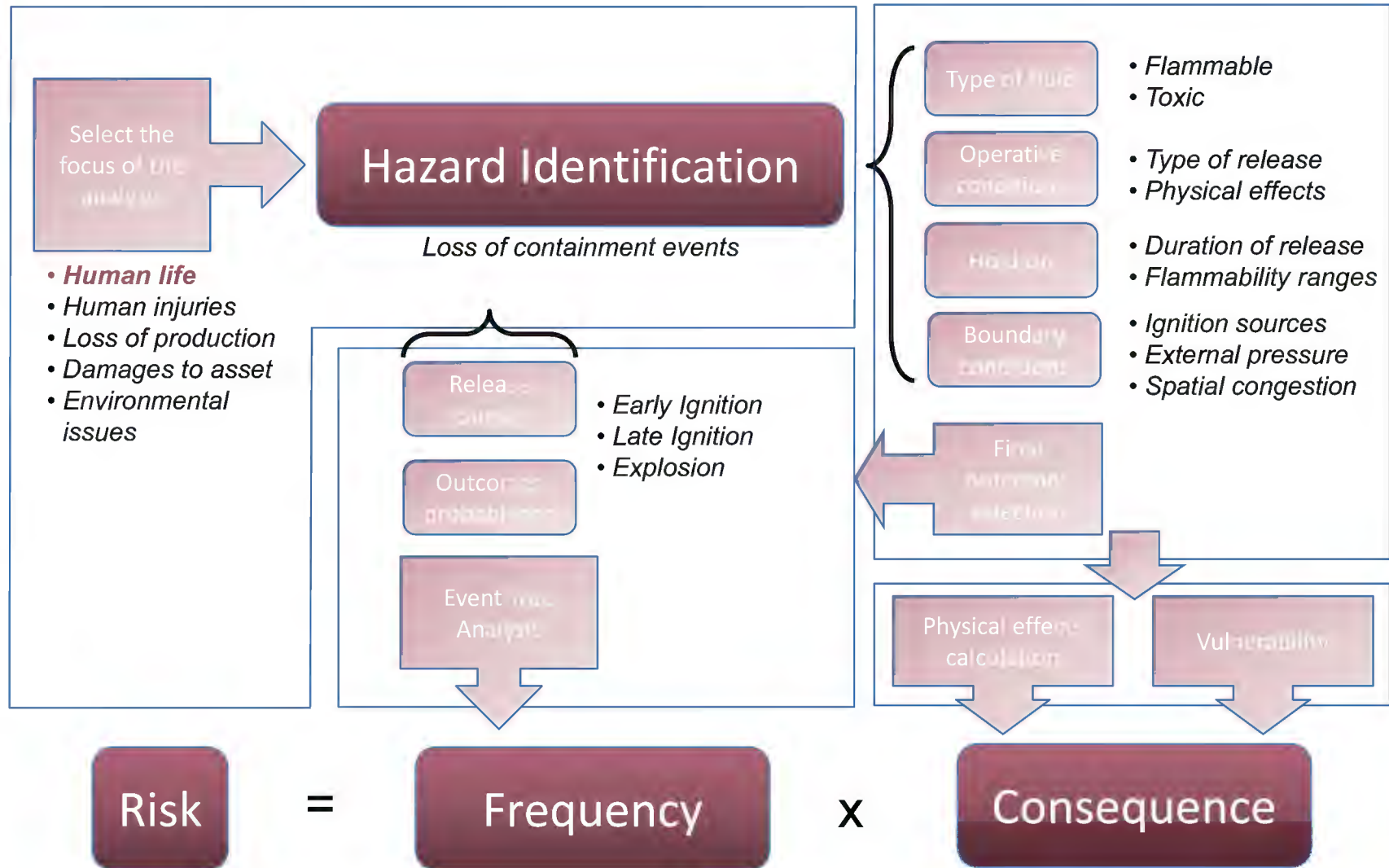
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Nabucco Gas Pipeline overview



- 4,000 km total length
- Different piping classes for feeders, Marmara crossing and main pipeline
- Large range of terrain types
- Pressure profile
- Population density

Risk assessment

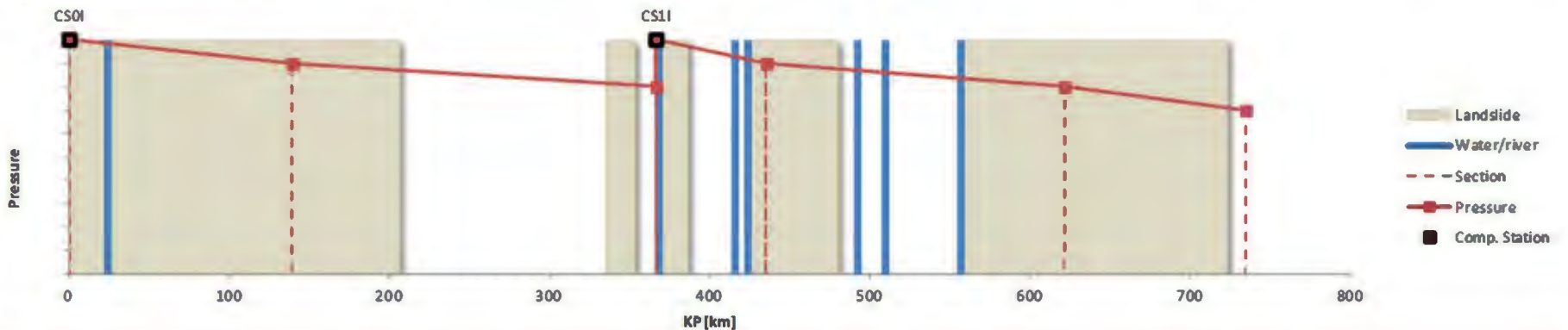
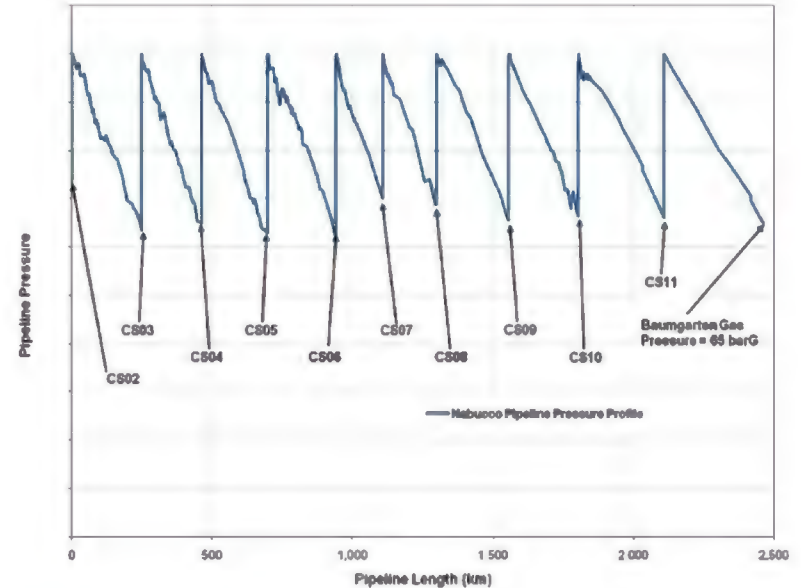


Hazard Identification

Onshore pipeline

- Corrosion and material defects
- Construction defects
- Ground movement
- Other and unknown

- Operative conditions (mainly pressure) vary along the pipeline
- Different gas composition in the feeders
- Land use and terrain conformation
- 3 hole sizes (pinhole, hole, rupture)
- 47 section identified
- Identification of potential causes is performed based on published literature (EGIG)

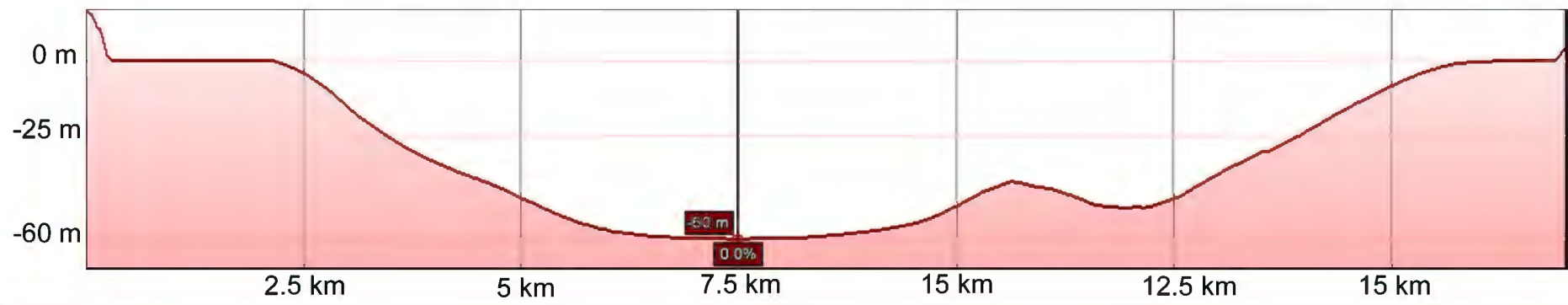
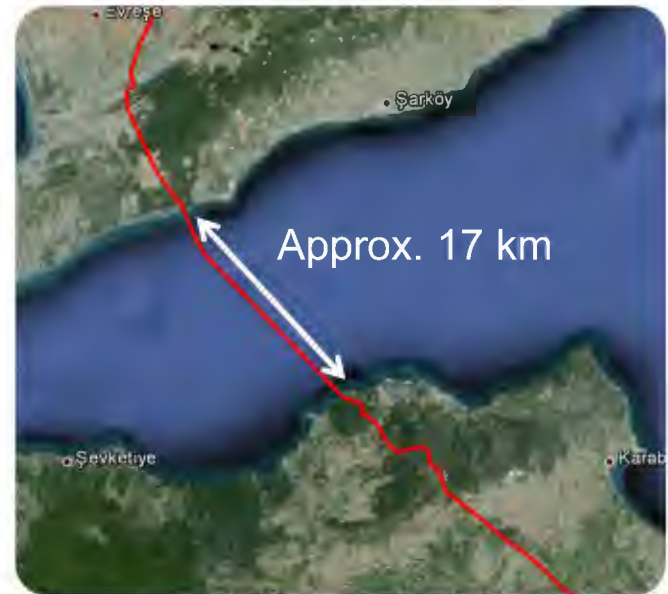


Hazard Identification

Offshore pipeline

- Corrosion and material defects
- Sinking ship
- Dropped objects
- Dropped or dragged anchors
- Fishing activities

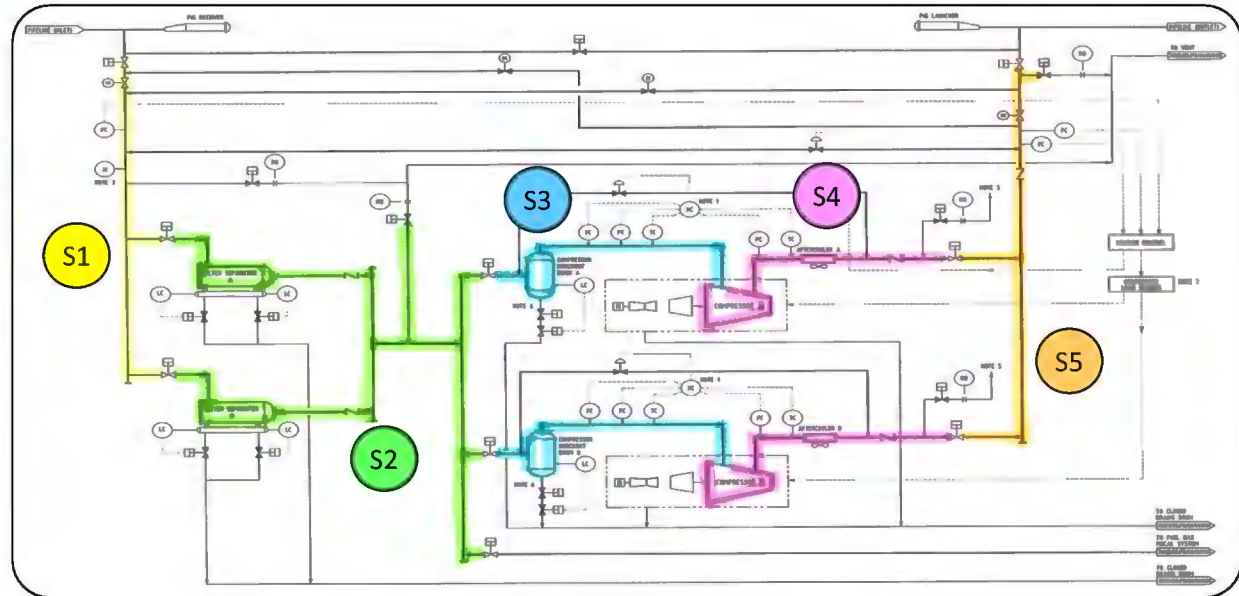
- Marmara crossing
- 17 River crossings
- 2 hole size (small breach and large breach)
- Identification of potential causes based on DNV-RP-F107 and PARLOC
- Maximum depth: 60 m
- 2 parallel lines
- High vessel traffic



Hazard Identification

Compressor station

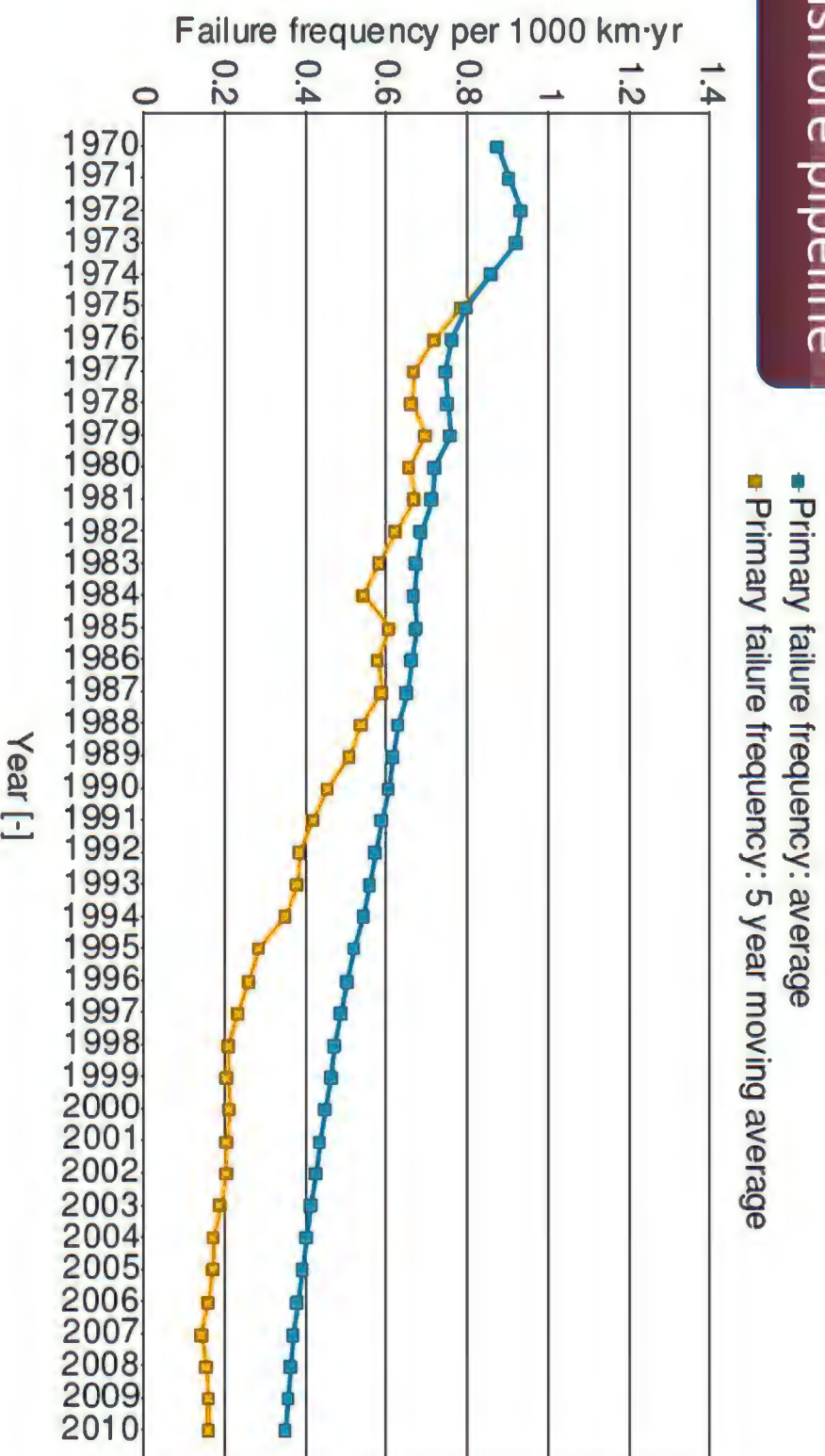
- Process deviations
- Random ruptures



- Compressor boost gas pressure
- UG/AG sections
- In building/Outside building
- Isolatable section (hold-up)
- Two hole sizes (1" and 4")
- Identification of potential causes based on API 581

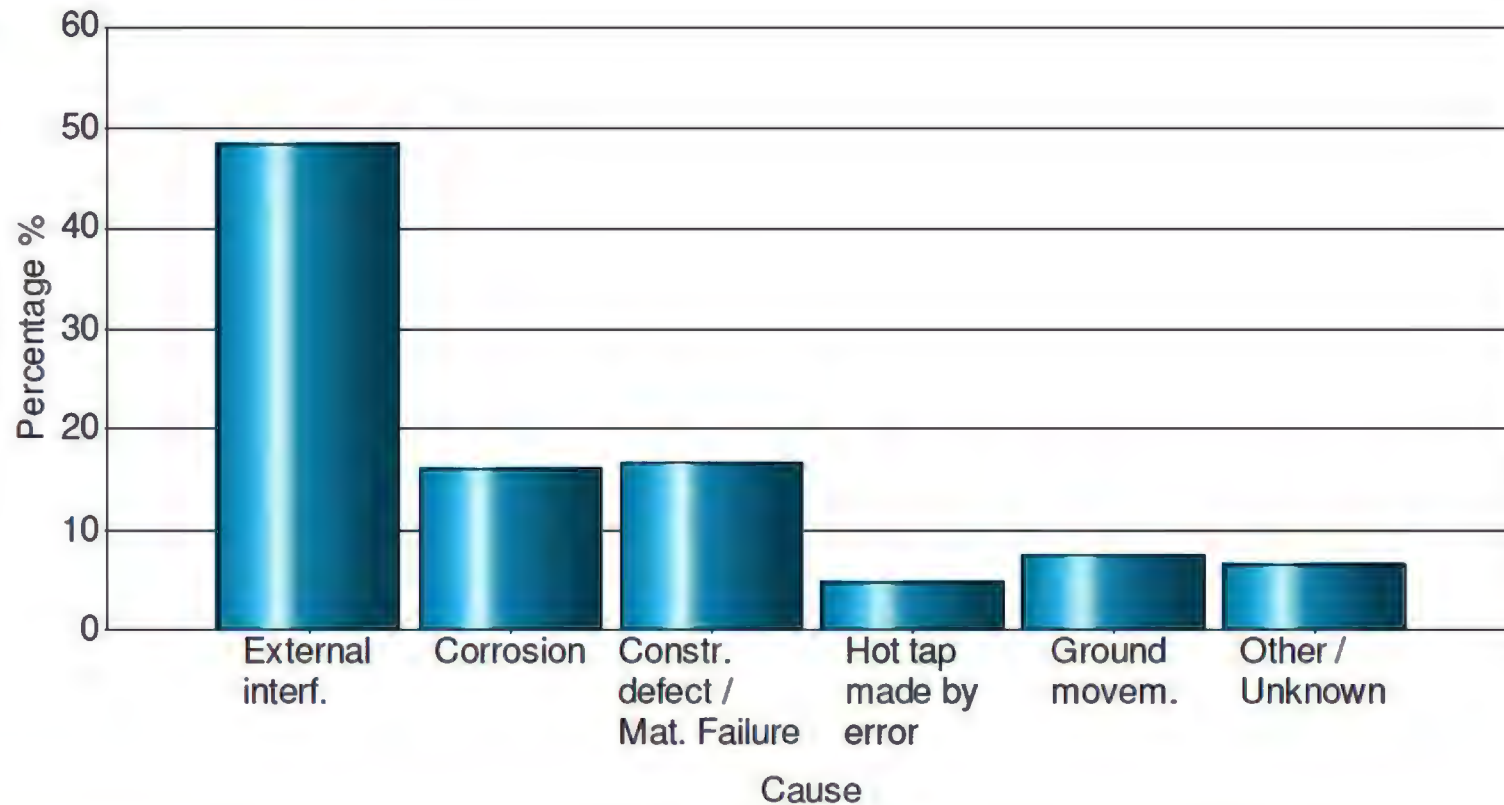
Frequency assessment

Onshore pipeline



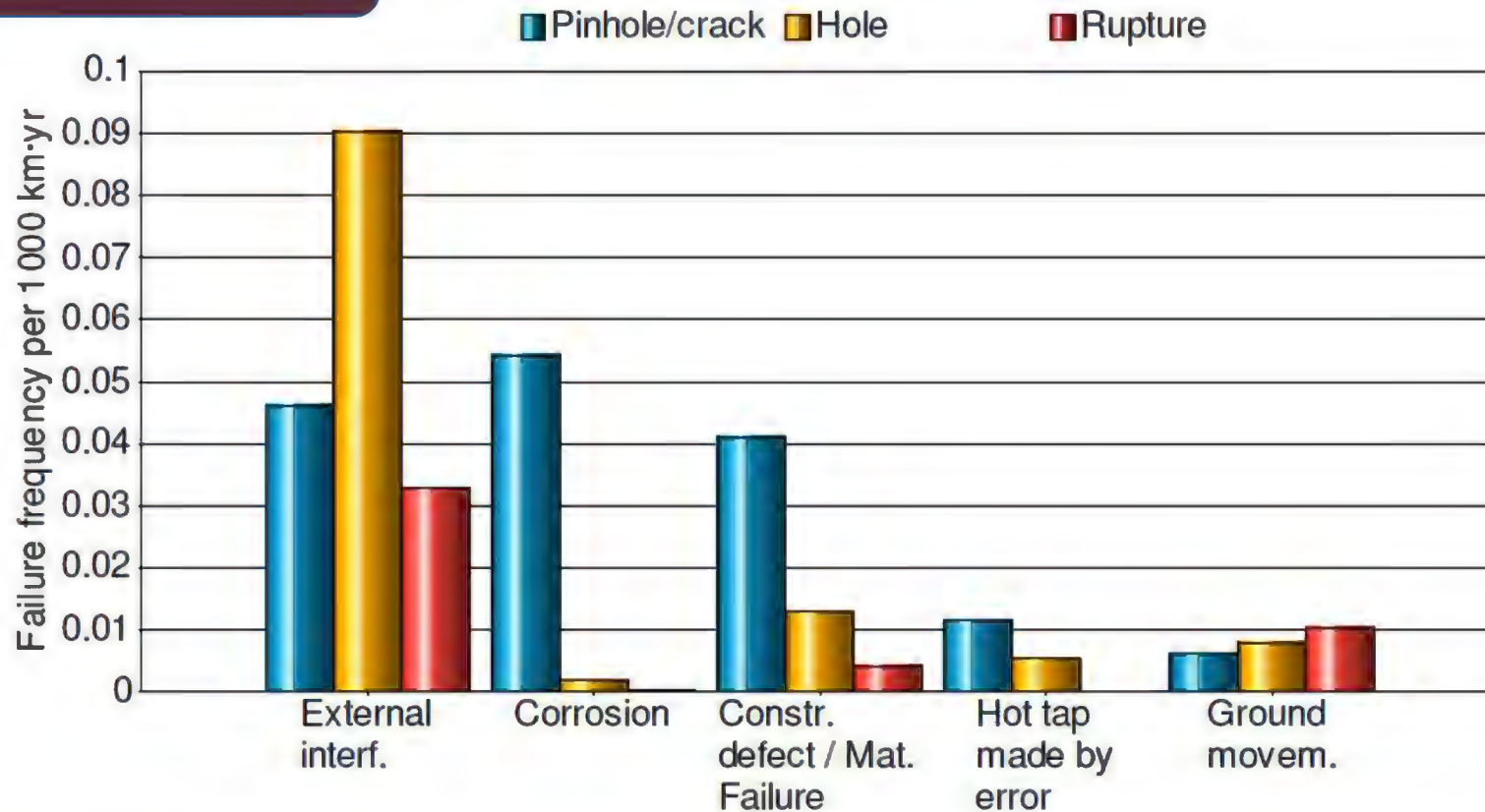
Frequency assessment

Onshore pipeline



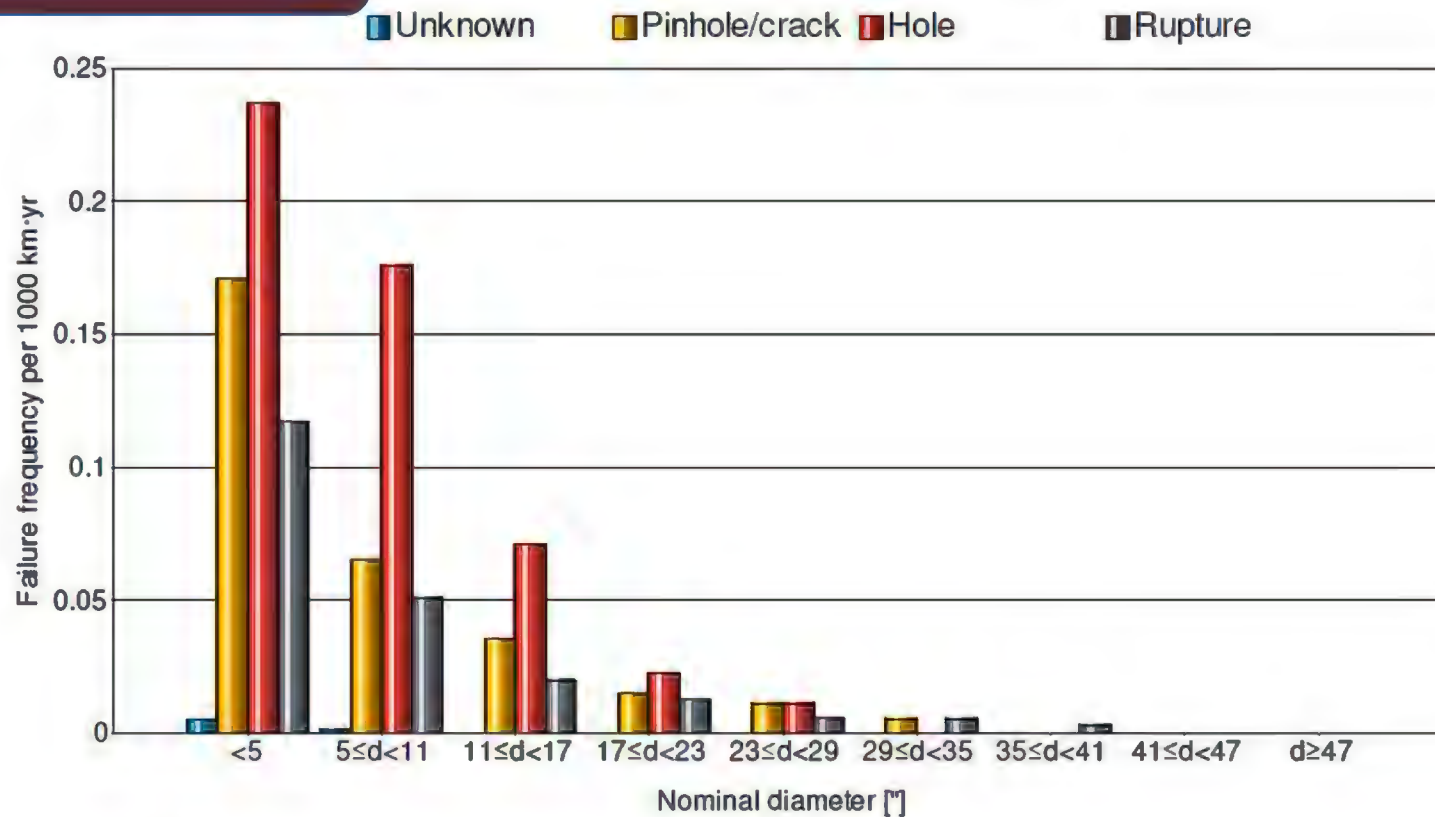
Frequency assessment

Onshore pipeline



Frequency assessment

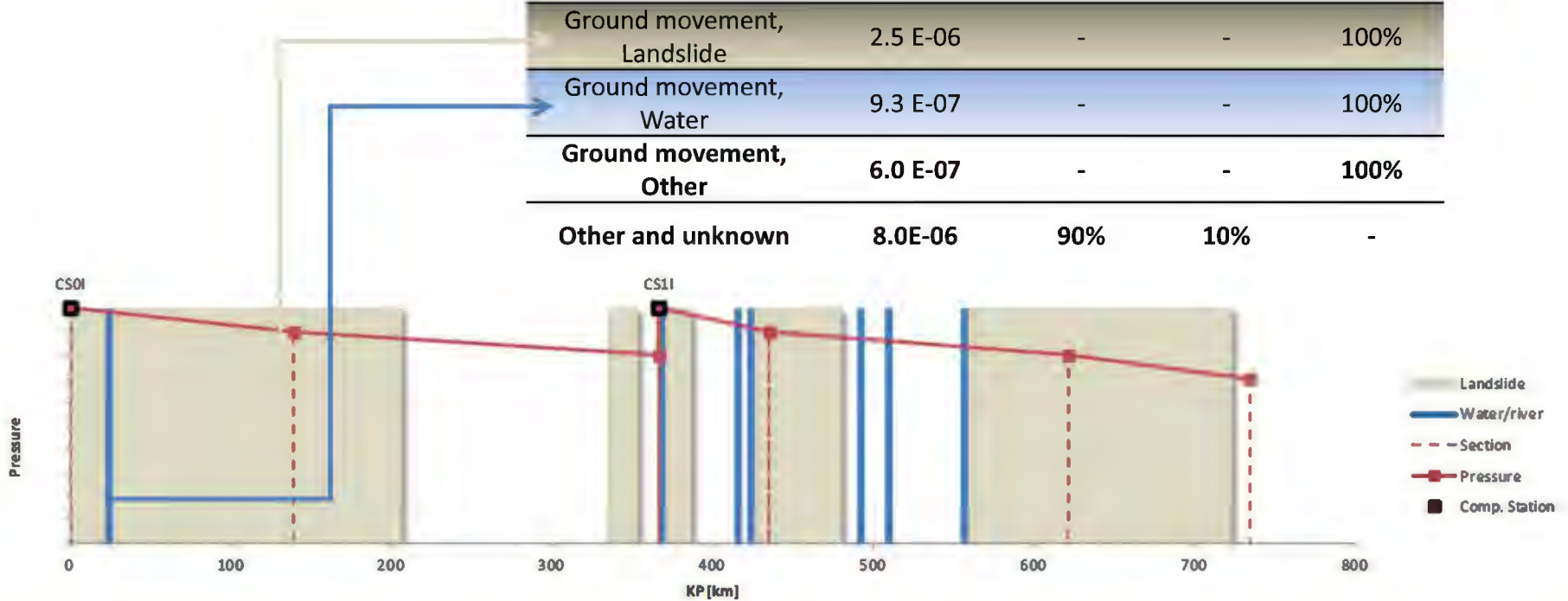
Onshore pipeline



Frequency assessment

Onshore pipeline

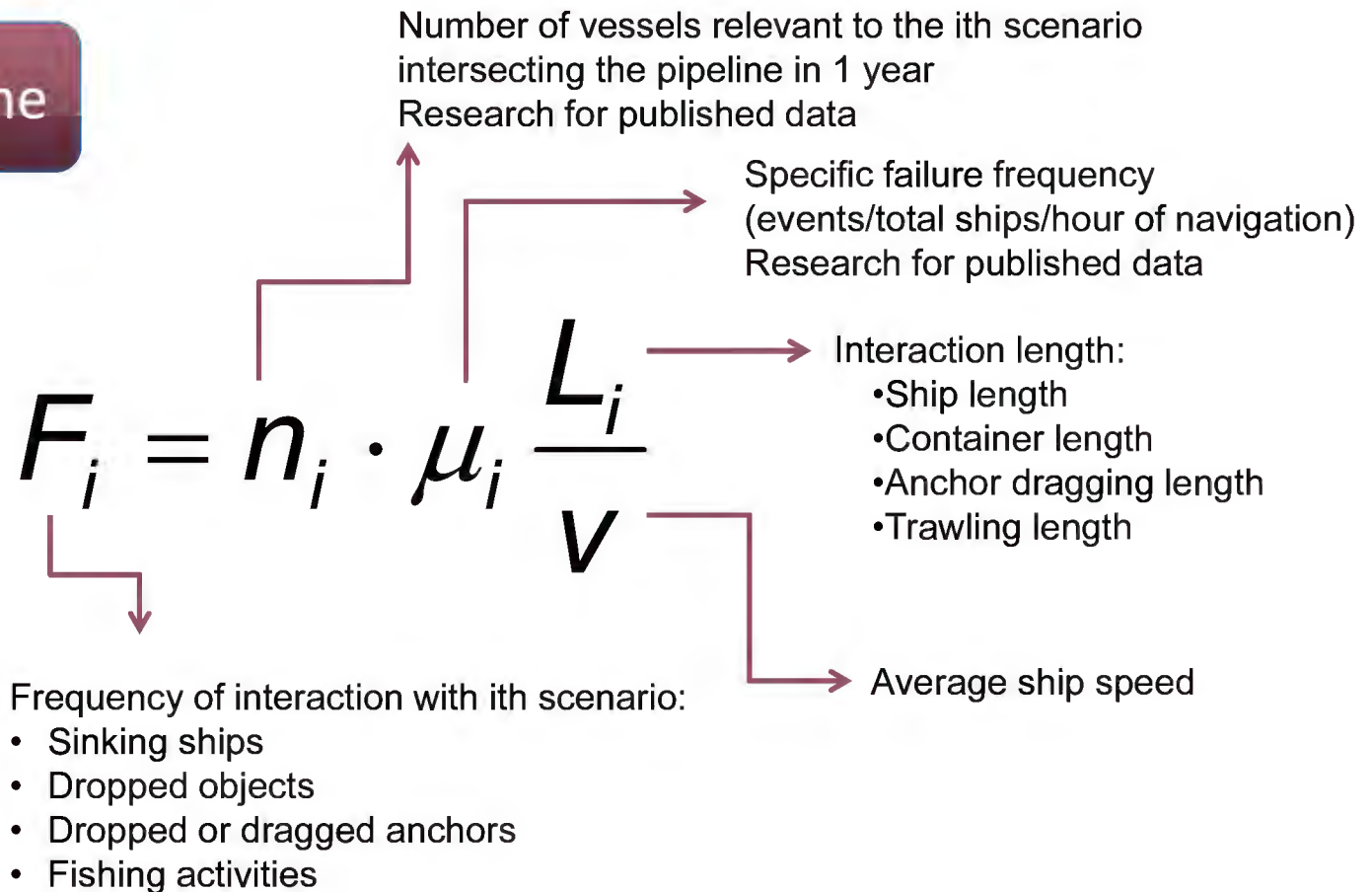
Cause	Frequency [ev/km/yr]	Pinhole	Hole	Rupture
<i>External interference</i>	-	-	-	-
<i>Corrosion</i>	-	-	-	-
Construction defect/ Material failure	3.1E-05	71%	22%	7%
<i>Hot tap made by error</i>	-	-	-	-
Ground movement, Landslide	2.5 E-06	-	-	100%
Ground movement, Water	9.3 E-07	-	-	100%
Ground movement, Other	6.0 E-07	-	-	100%
Other and unknown	8.0E-06	90%	10%	-



Frequency assessment

Offshore pipeline

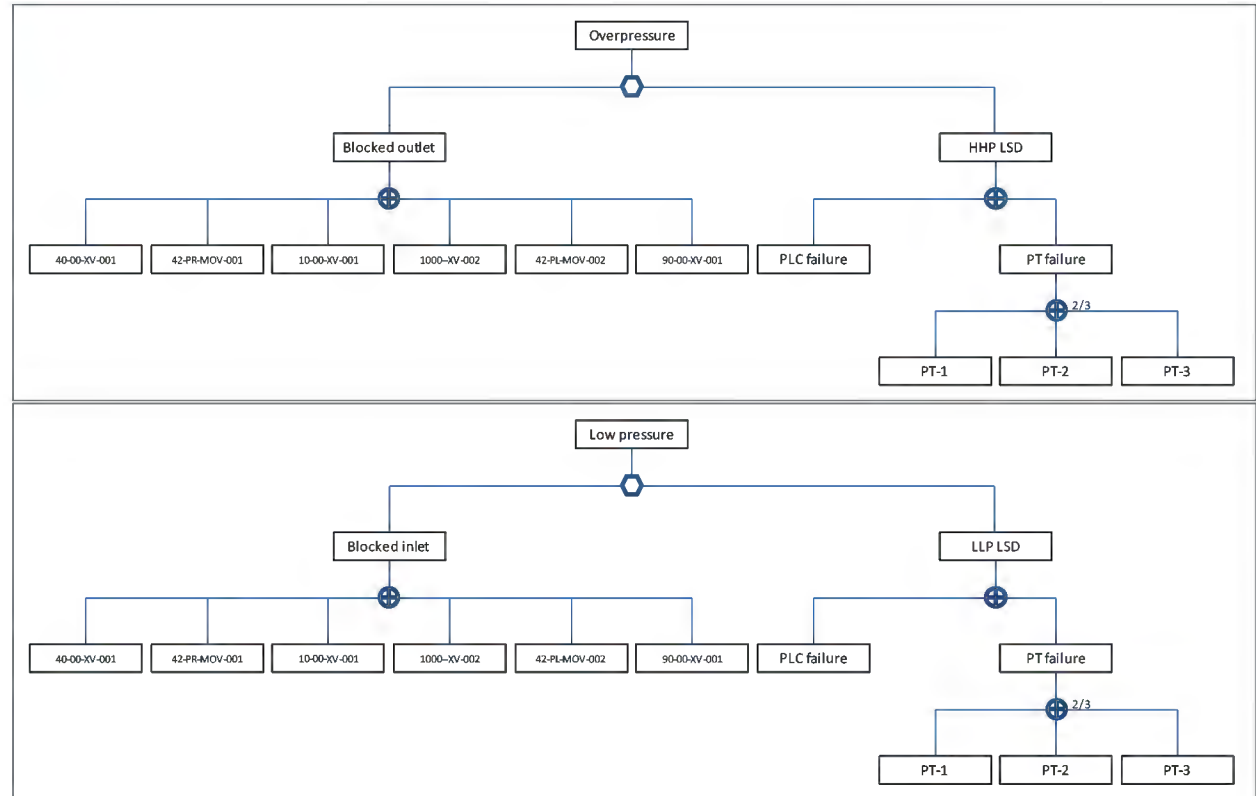
- Internal causes are assessed through specific frequency databases (PARLOC)
- Interactions with third parties are assessed through dedicated models



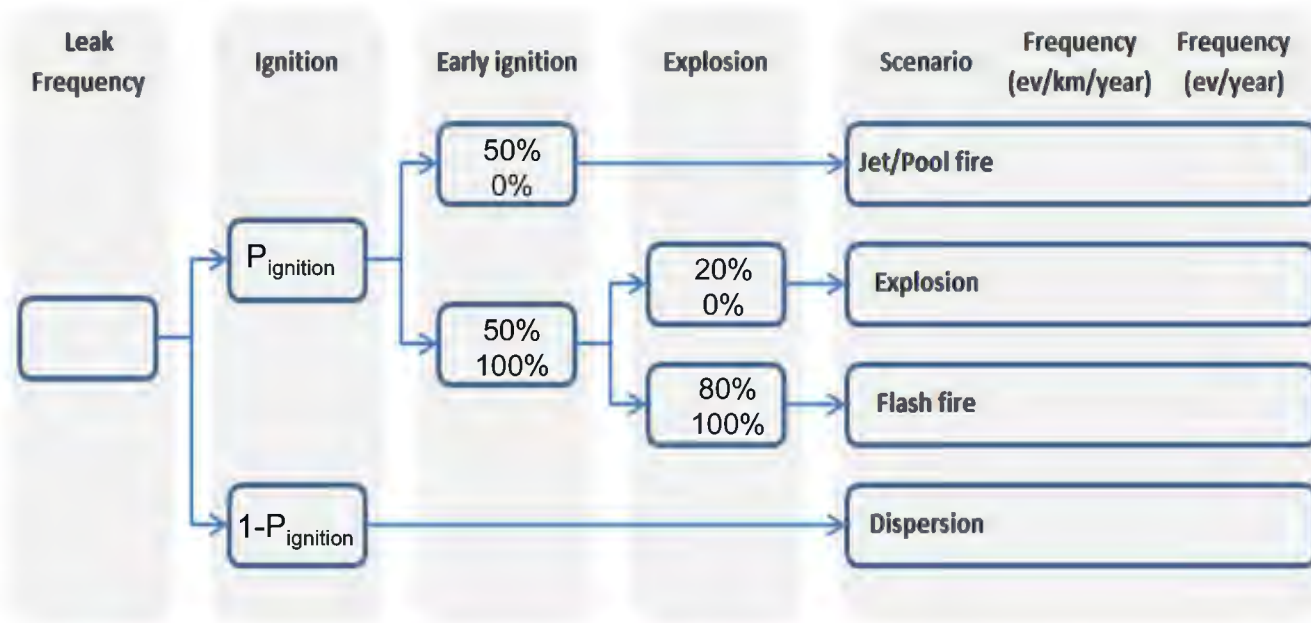
Frequency assessment

Compressor station

- Internal causes are assessed through specific frequency databases (API 581)
- Process deviations are assessed through Fault Tree Analysis



Event tree analysis

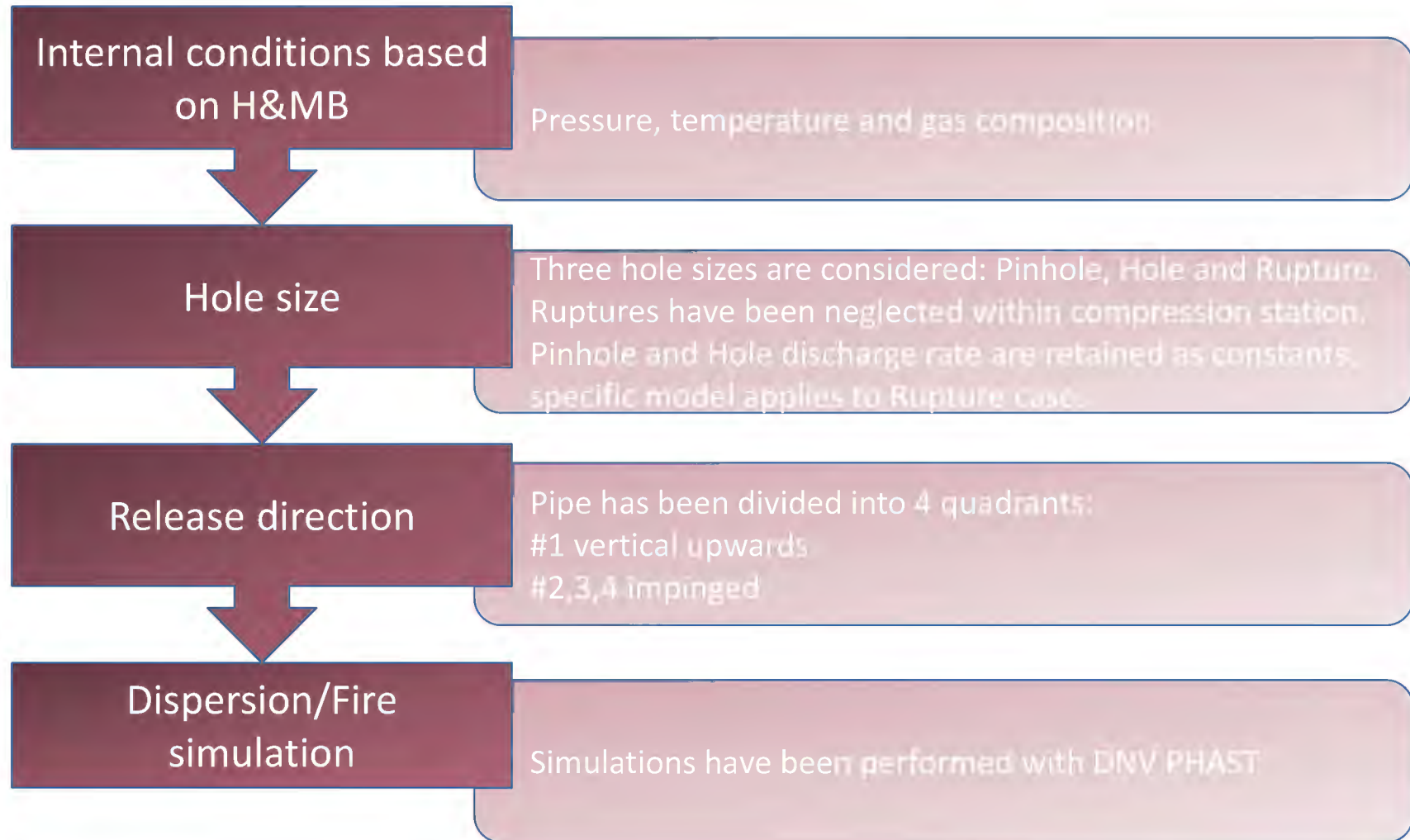


Onshore ignition probability $P_{\text{ignition}} = 10^{0.64 \cdot \text{Log}_{10} \dot{M} - 1.81}$

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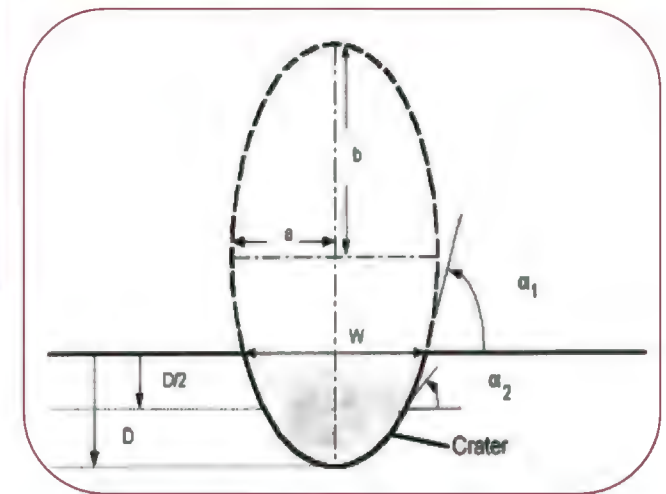
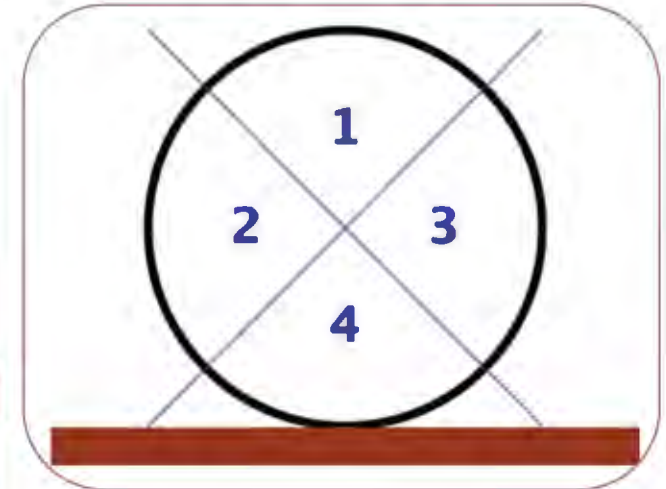
Offshore ignition probability $P_{\text{ignition}} = \frac{L_{\text{cloud}}}{V} \cdot n_{\text{vessel}} \cdot \frac{L_{\text{cloud}}}{L_{\text{strait}}}$

Consequence assessment (onshore)



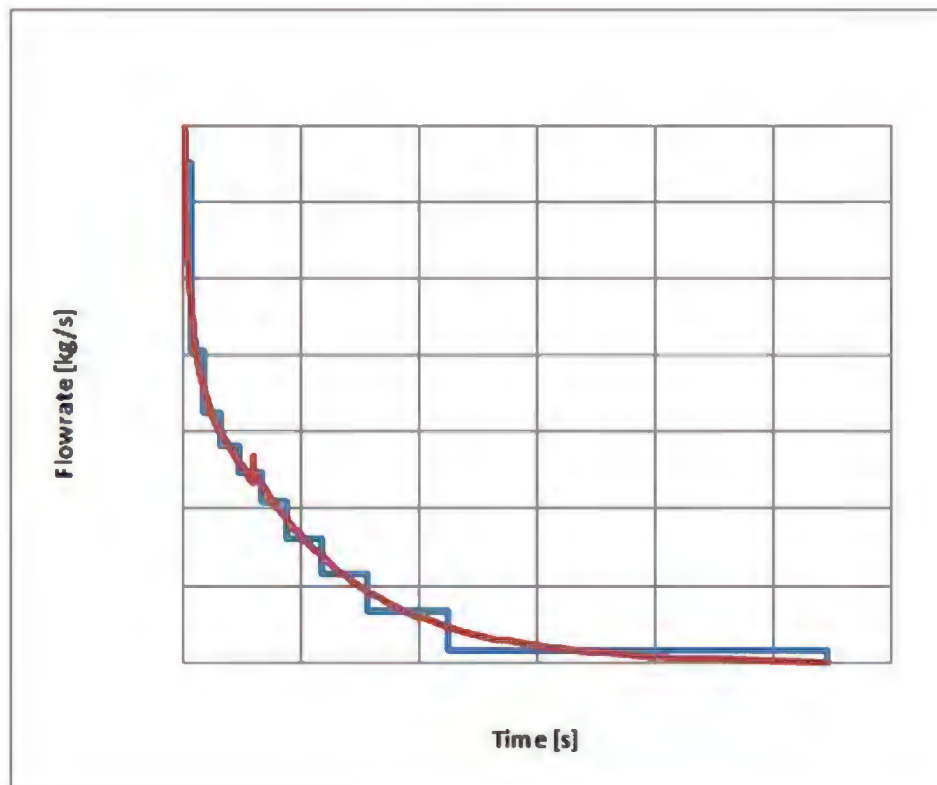
Consequence assessment (onshore)

Hole size Quadrant	Pinhole	Hole	Rupture
#1	Impinged (minimum gas velocity)	Vertical upward	Crater formation
#2, 3, 4	Impinged (minimum gas velocity)	Impinged (minimum gas velocity)	



Consequence assessment (onshore)

Full bore rupture release rate

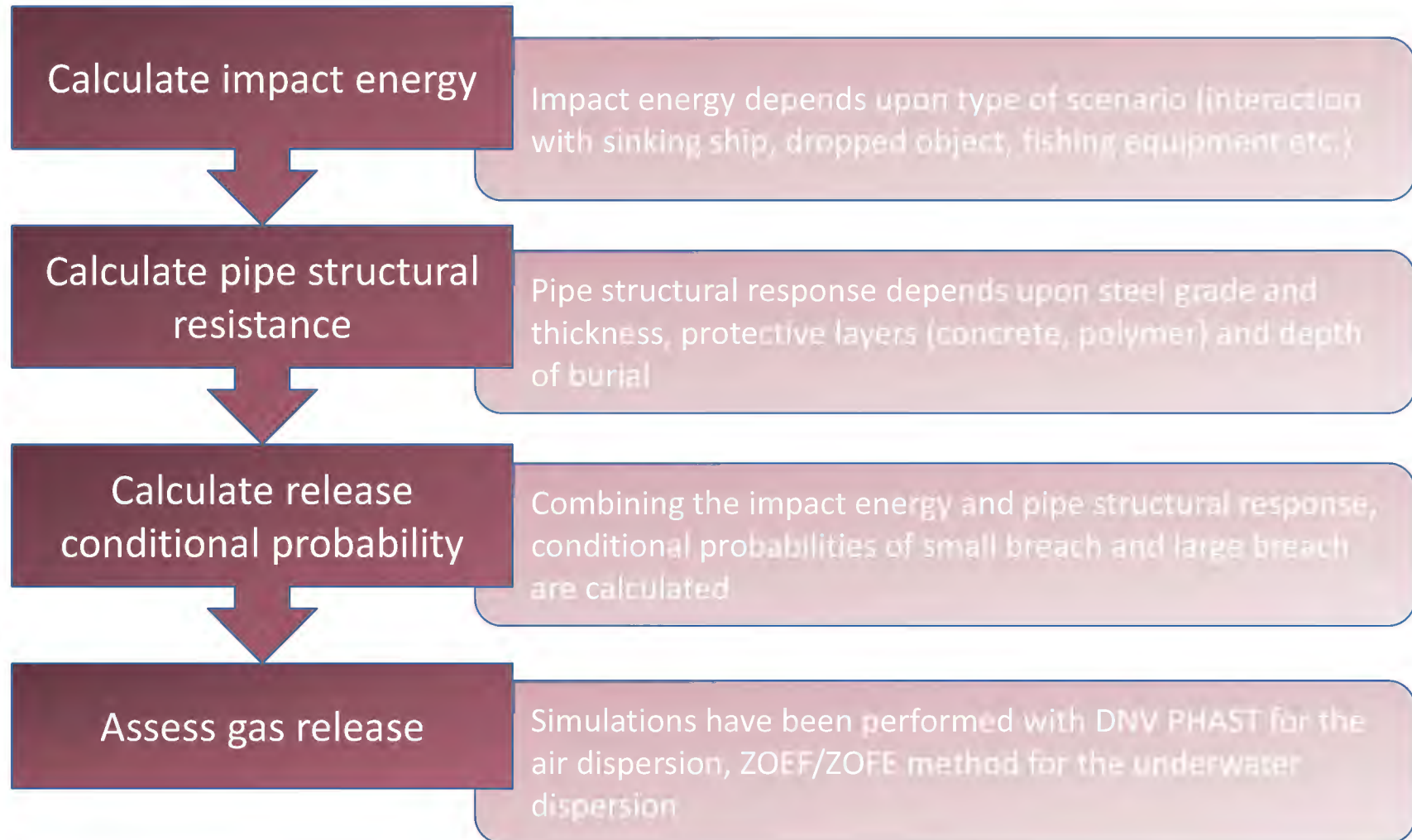


Blue line represents the interpolation steps used in dispersion evaluation

Red line represents the discharge flow rate evaluated by Long pipeline model in PHAST

For Jet fire calculation, flow rate at 30 second has been selected

Consequence assessment (offshore)



Consequence assessment (offshore)

$$E_E = \frac{1}{2} \cdot (m + m_a) \cdot v^2$$

$$v = \sqrt{\frac{2 \cdot m_i \cdot g}{\rho_{water} \cdot C_D \cdot A_i} - \frac{2 \cdot g \cdot V_{a(i)}}{C_D \cdot A_i}}$$

- m : mass of the sinking object (ship, container, anchor)
- V_a : volume of the sinking object
- A_i : projected area of the sinking object in the flow direction
- C_d : drag coefficient
- g : gravitation acceleration

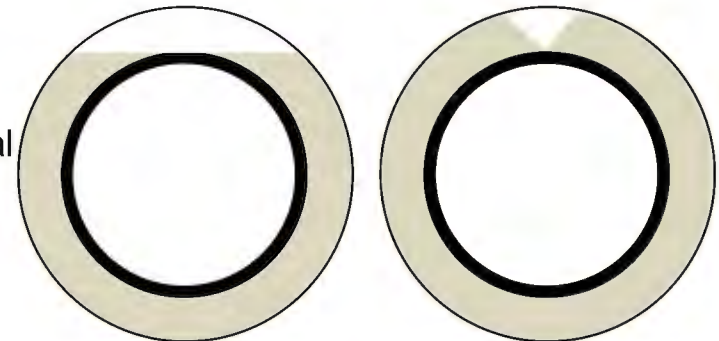
$$E_D = 16 \cdot \left(\frac{2 \cdot \pi}{9}\right)^{\frac{1}{2}} \cdot m_p \cdot \left(\frac{D}{t}\right)^{\frac{1}{2}} \cdot D \cdot \left(\frac{\delta}{D}\right)^{\frac{3}{2}}$$

- E_D : absorbed energy for steel pipelines
- m_p : plastic moment capacity of the wall ($\frac{1}{4} \sigma_y t^2$)
- δ : pipe deformation, dent
- t : wall thickness (nominal)
- σ_y : yield stress
- D : steel outer diameter

$$E_K = Y \cdot V_P$$

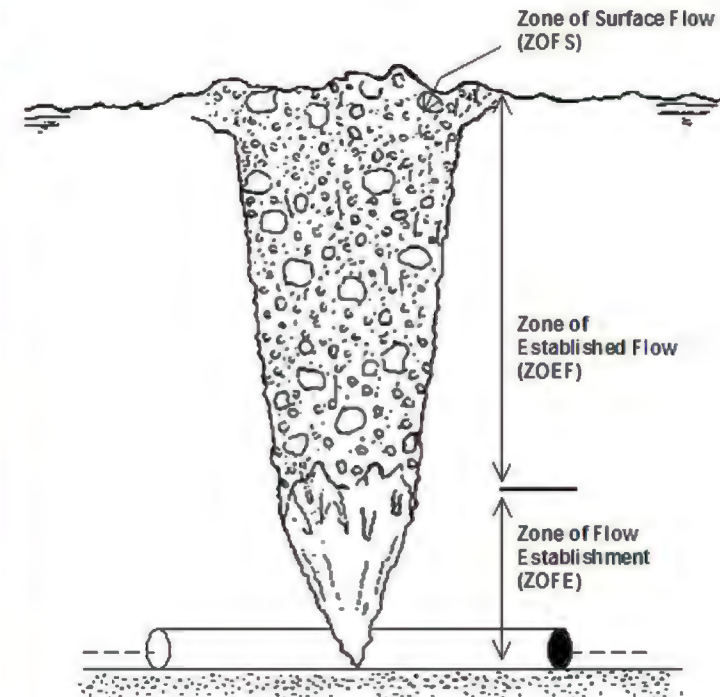
$$E_P = \frac{2}{3} \cdot \gamma' \cdot L \cdot N_\gamma \cdot z^3$$

- Y : crushing strength of the concrete
- V_P : penetrated volume (m^3).
- γ' : effective unit weight of the fill material
- L : length of the impacting side (m);
- N_γ : bearing capacity coefficient
- z : penetration depth (m).

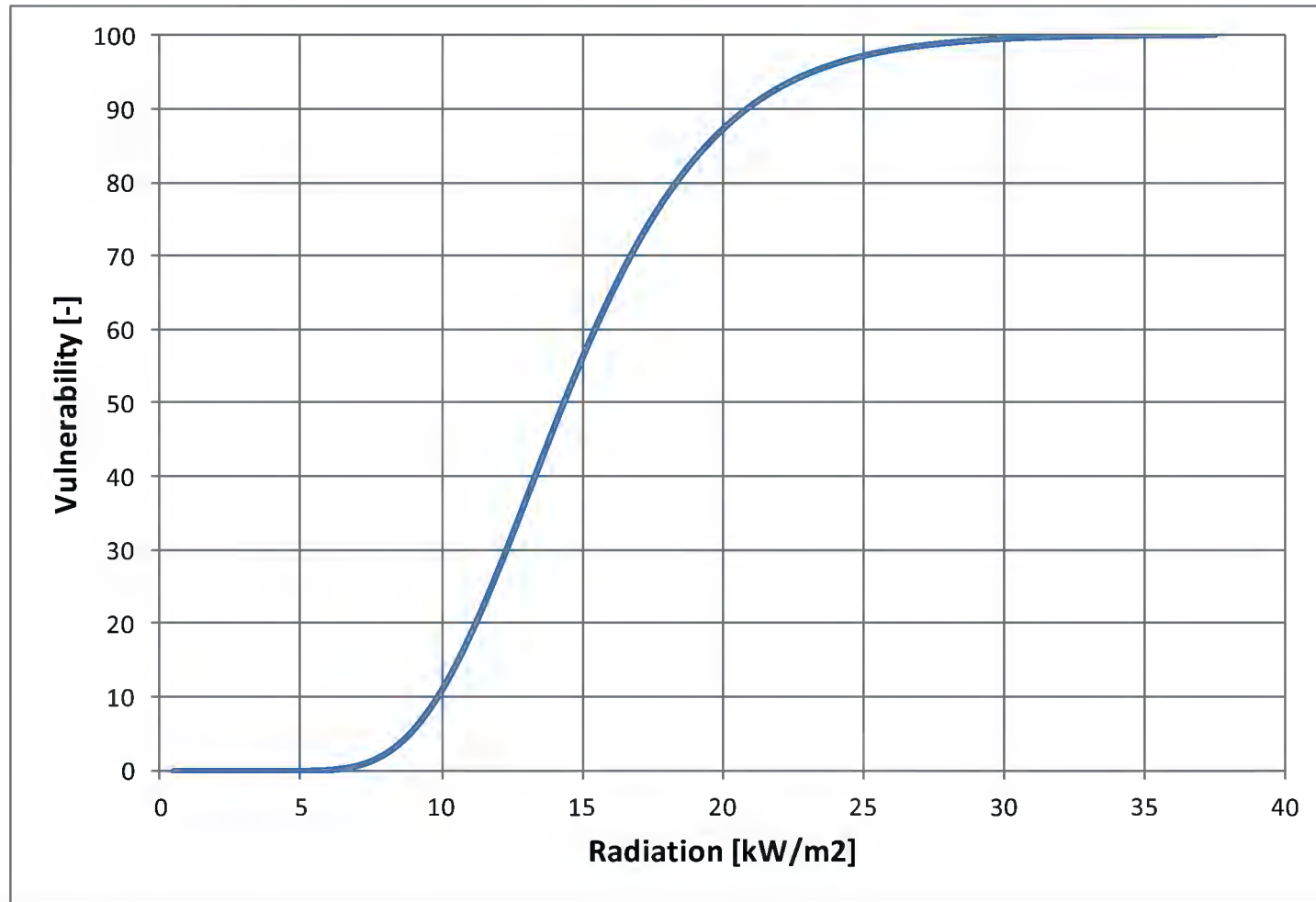


Consequence assessment (offshore)

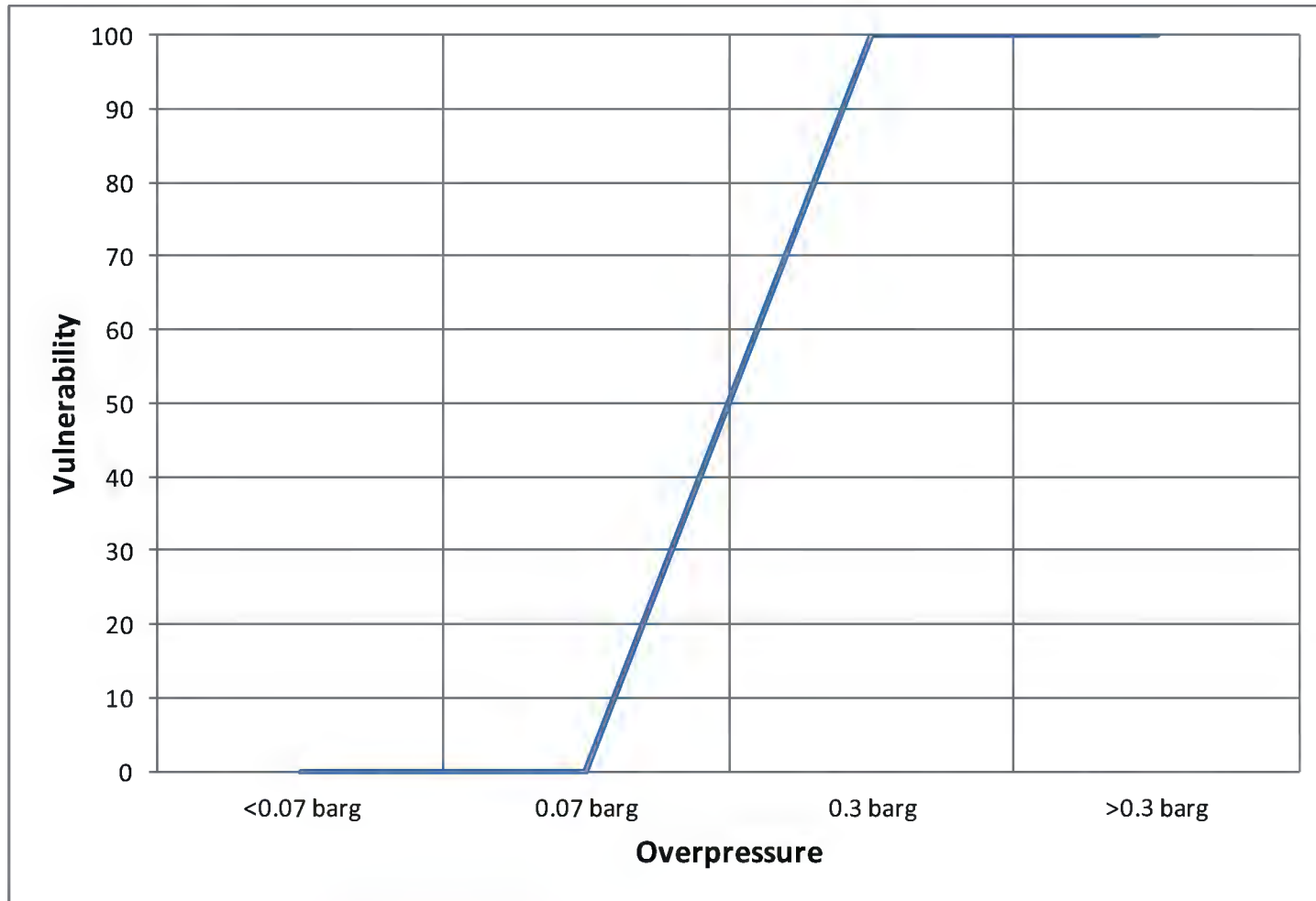
DENT/ DIAMETER (δ/D , in %)	DAMAGE DESCRIPTION (Ref. DNV-RP-F107)	CONDITIONAL PROBABILITY	
		Small breach	Large breach
< 5	Minor damage. No release	0	0
5 – 10	Major damage. Small Release possible	0.1	0
10 – 15	Major damage. Release possible Small releases more likely than large releases	0.2	0.05
15 – 20	Major damage. Release possible Small releases more likely than large releases	0.5	0.25
> 20	Major damage. Release possible Large releases more likely than small releases	0.2	0.7



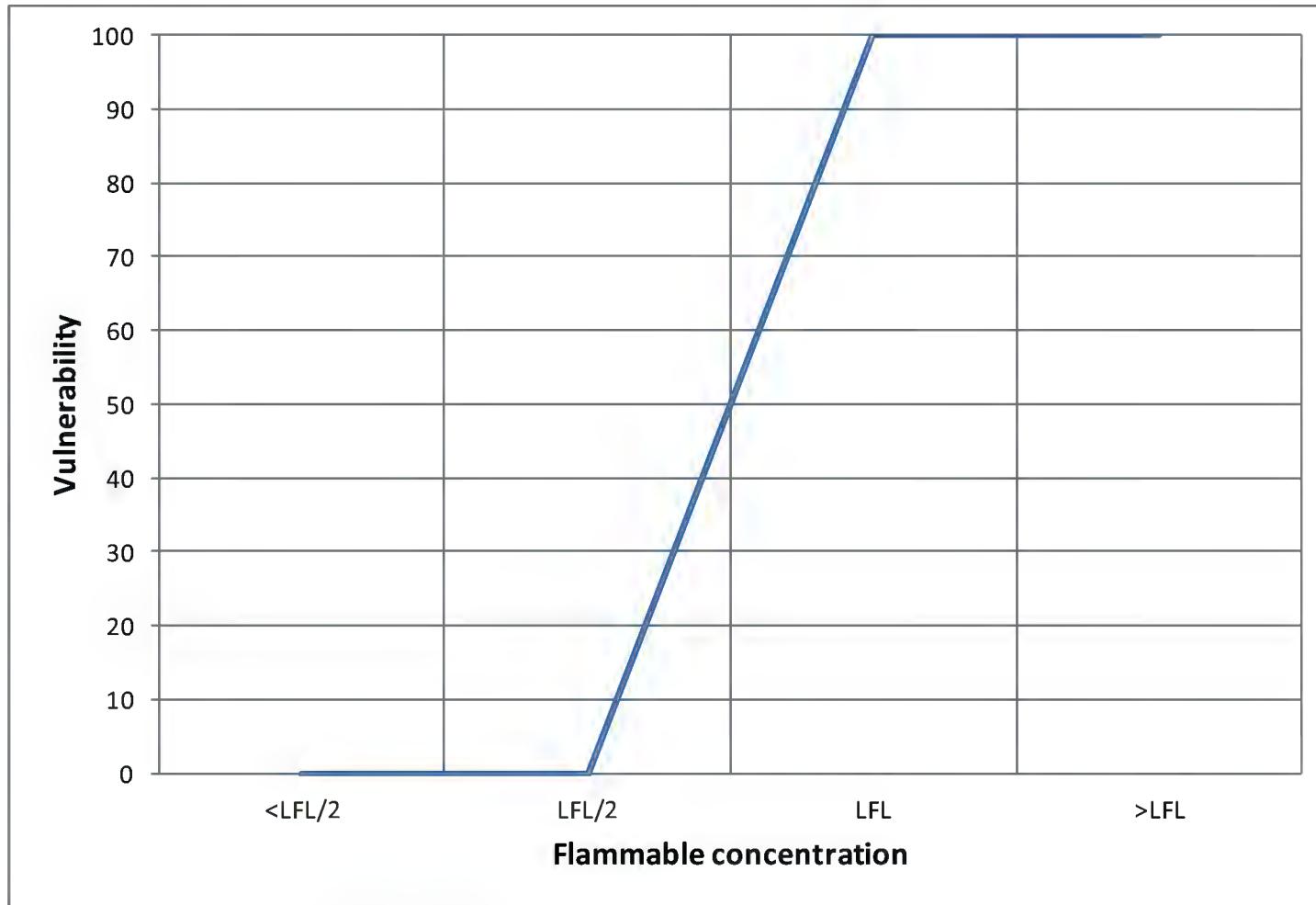
Vulnerability



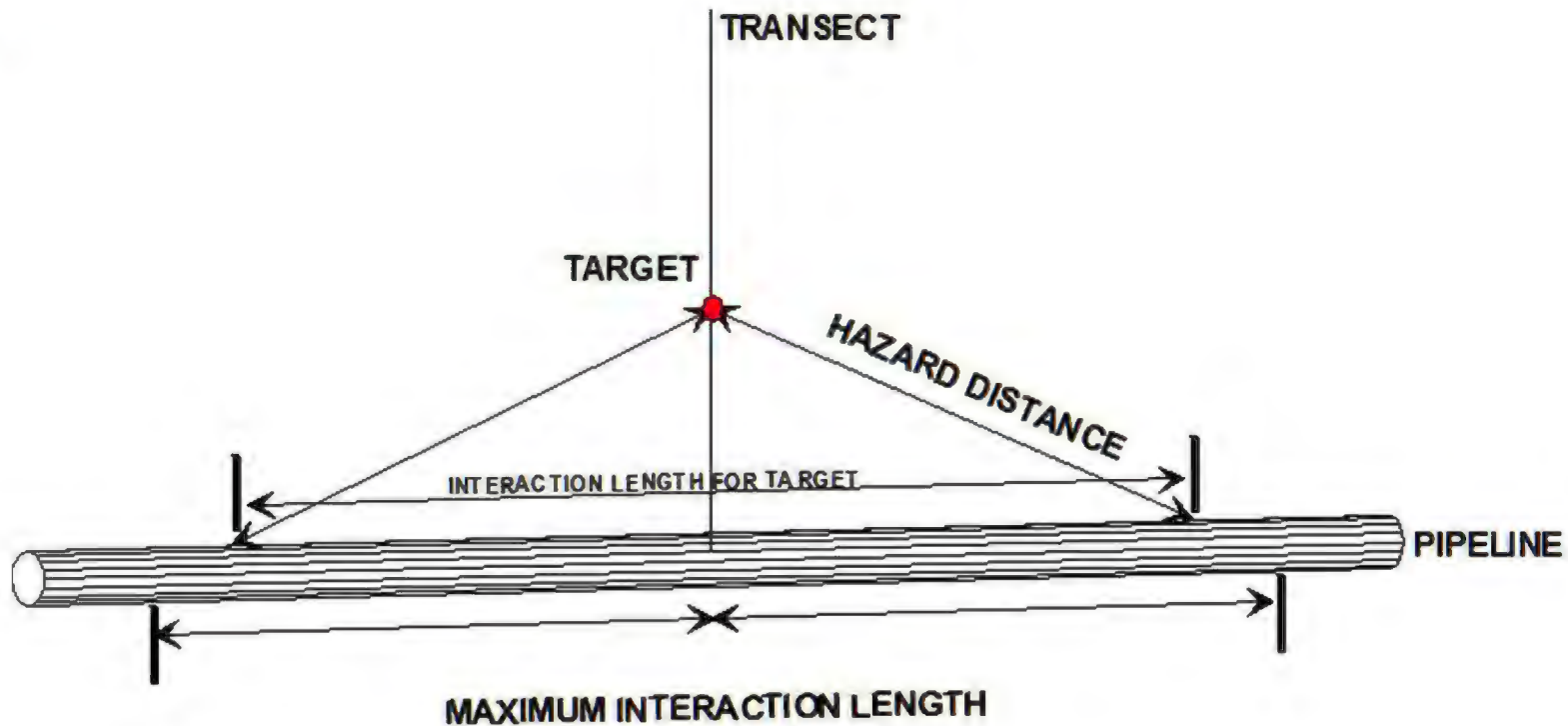
Vulnerability



Vulnerability

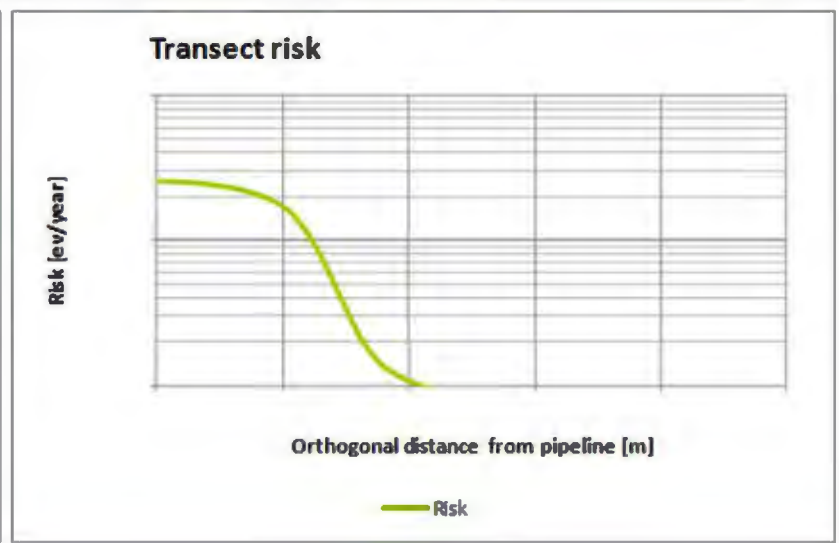
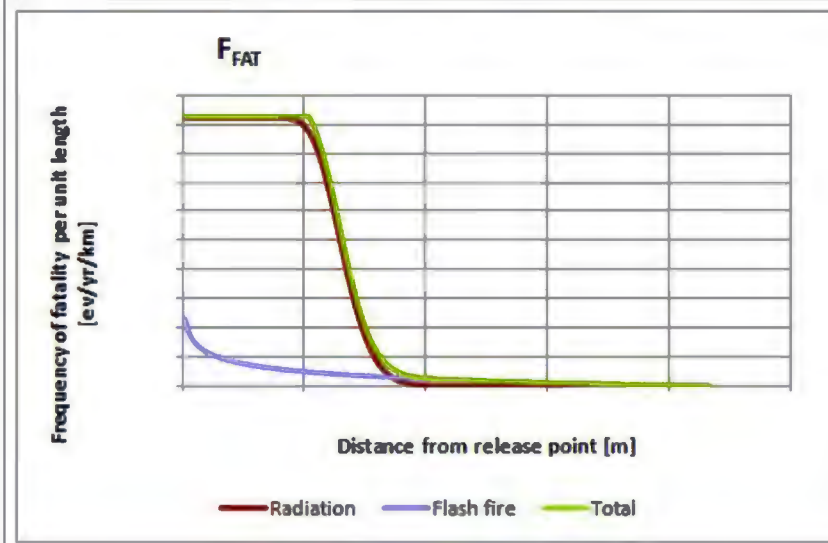
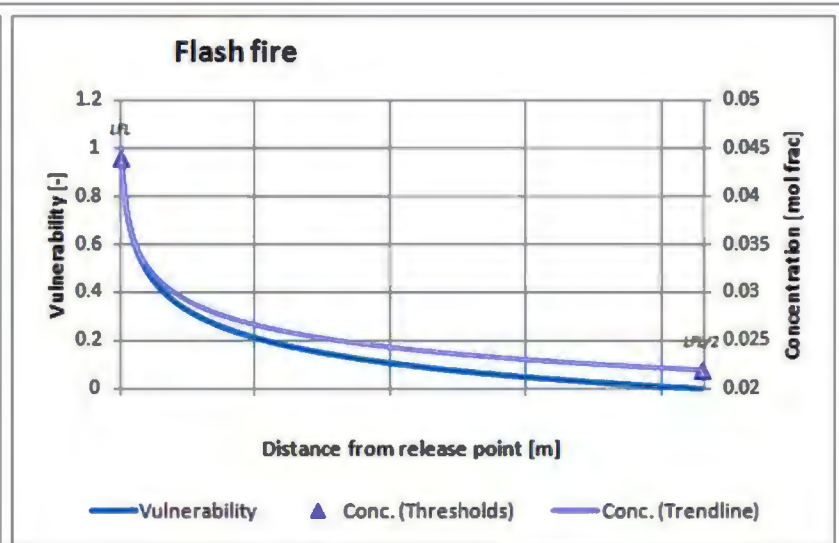
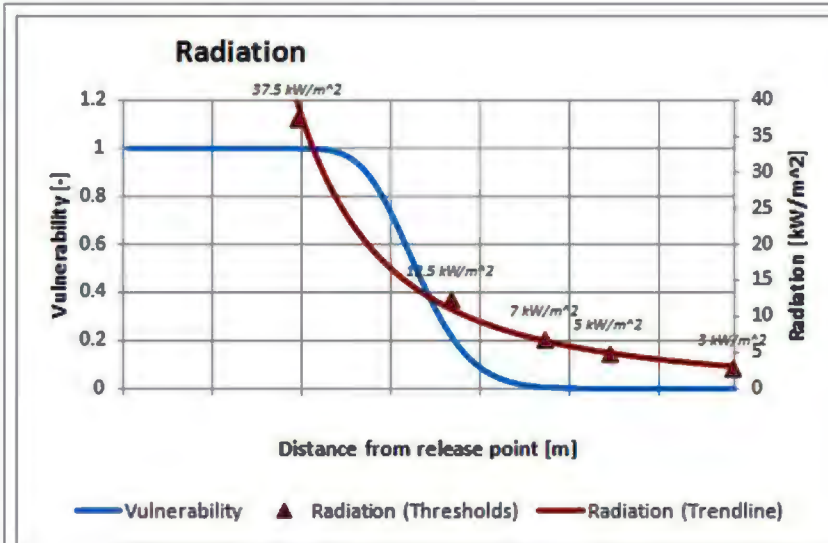


Individual risk



- LSIR (Location Specific Individual Risk): risk of death for an individual who is present at a particular location 24 hours per day and 365 days per year
- Interaction length concept is introduced in order to evaluate the pipeline length able to affect a specific location

Individual risk



Individual risk

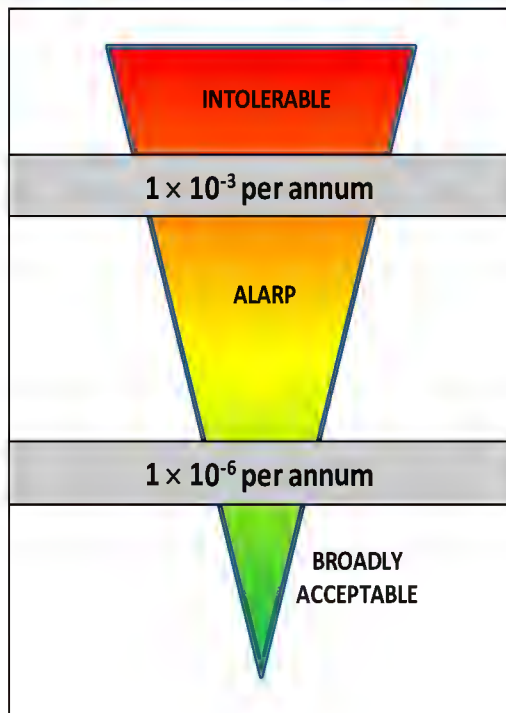


Single scenario risk



Tolerability criteria

Quantitative



Semi-quantitative

Frequency	Consequence Level				
	1	2	3	4	5
Improbable	Acceptable region				
Unlikely				Acceptability limit	
Seldom			ALARP region	Tolerability limit	
Probable					
Frequent					Intolerable region

Conclusions

- A QRA were performed for the Nabucco pipeline
- Risk assessment is performed through the following steps:
 - Hazard identification
 - Frequency calculation
 - Consequences calculation
 - Risk calculation and assessment
- Boundary conditions vary along the pipeline, thus requiring several different approaches to model risk
- Data searching is a key factor in risk assessment
- Assumptions based on the expert know-how still apply

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D'Appolonia S.p.A.

Headquarters:

Via San Nazaro, 19

16145 Genova – Italy

Tel. +39 010 3628148 Fax +39 010 3621078

email: dappolonia@dappolonia.it

website: www.dappolonia.it